RUHANIA / Chemical Technology. Food Industry.

H-28

Abs Jour : Ref. Zhur-Khimiya, No 12, 1958, 41327.

Author

: Ionosku, Ivenesku, Poposku.

Inst

: Agricultural inst.

Titlo

: Application of corn flour in broad baking.

Orig Pub : Anuarul lucrar stiint, Inst, agron,, 1957, 179-190

Abstract: Experimental broad baking from mixtures of wheat and corn flour showed that best results were obtained with wheat flour \leq 85% yield with an addition of the corn flour (fine milling, of \leq 40% yield) in the amount not exceeding the

amount of the sifted off bran.

Card 1/1

APPROVED FOR RELEASE: 03/20/2001 CIA-RDP86-00513R000619320002-8"

IVENSE!, P.A.

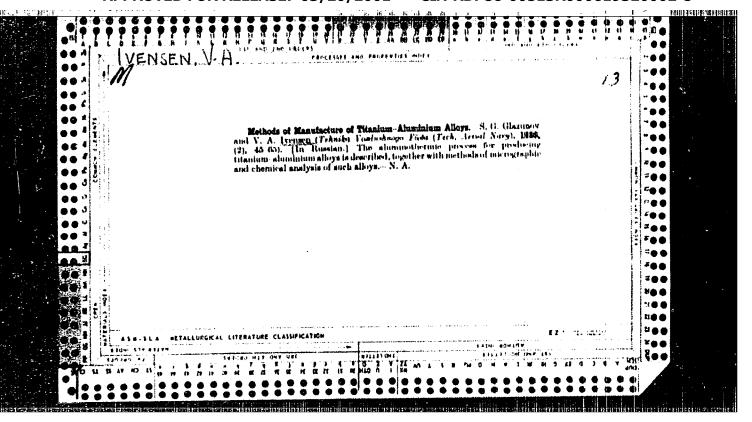
Remote control of mine loading and transfer points. Nauch, rab.
(VUGI no.11:75-91 '54.

1. Chelyabinskiy filial, Vsesoyuznyy nauchnoiseledovatel'skyy
institut.
(Remote control) (Mine haulage)

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KASHIRTSEV, Arkadiy Sergeyevich. Prinimali uchastiye: TOLSTYKH, A.N.; IVENSEN, T.Yu.; UVAROV, S.V.. STEPANOV, D.L., prof., otv.red.; KORDE, K.B., red.izd-va; SUSHKOVA, L.A., tekhn.red.

[Field atlas of the fauna of Permian deposits in the northeastern part of the U.S.S.R.] Polevoi atlas fauny permskikh otlozhenii Severo-Vostoka SSSR. Moskva, Izd-vo Akad.nauk SSSR. 1959. 84 p. (MIRA 13:2) (Siberia, Eastern--Paleontology, Stratigraphic)

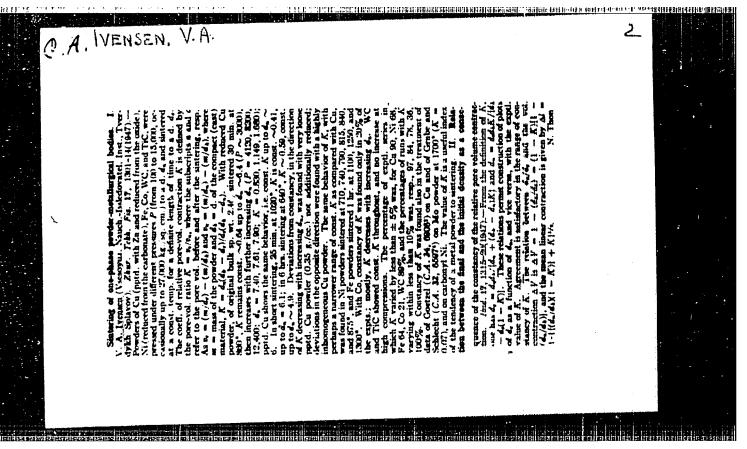


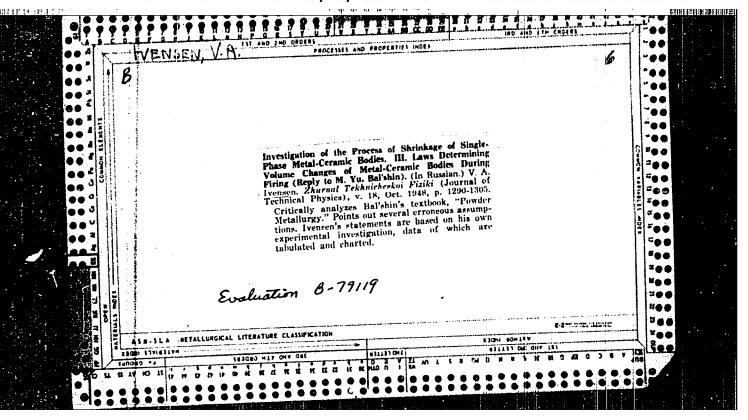
IVENSEN, V. A., Engr. and. Took. Sci.

Dissertation: "Investigation of the Compacting Process During Sintering Single-Fnase Metal Ceramic Products." Moscow Order of the Labor Red Panner Inst of Steel imeni

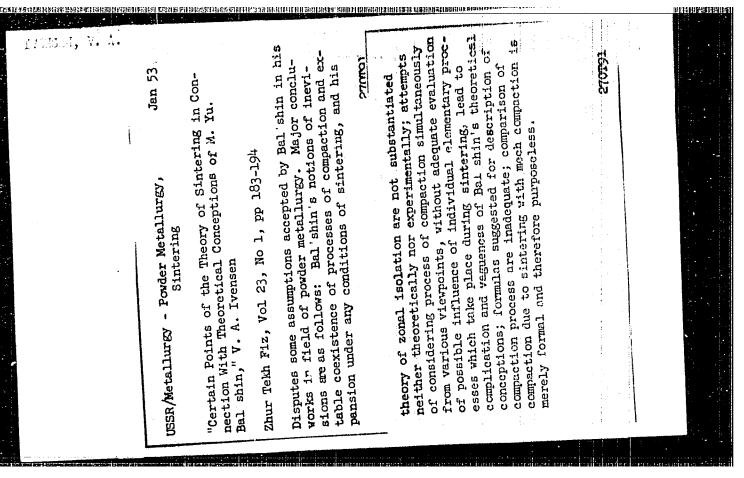
I. V. Stalin, 17 Jun 47.

SO: Vechernyaya Moskva, Jun, 1947 (Project #17836)





IVENSEN, V. A.	USSR/Metals - Sintering "Investigating the Consolidation of Metallo-Ceramic Materials During Sintering. VI. Difference in Behavior of Amorphous and Crystalline (Metallic) Porous Materials During Sintering," V.A. Ivensen "Zhur Tekh Fiz" Vol XXII, No 4, pp 677-685	र ४०० व	terials leads to a sharp change in the relation speeds of consolidating processes and processes enting the free energy. Received 6 Aug 51.	
	USSR/Metals "Investigat Materials D Behavior of Porous Mate	It was for during sand of pterials	materials of speeds lowering	



AUTHOR: Ivensen, V. A. SOV/126-6-2-32/34

TITLE: Discussion: On the Diffusion Theory of Sintering (Diskussiya: O diffusionnoy teorii spekaniya)

PERIODICAL: Fizika Metallov i Metallovedeniye, 1958, Vol 6, Nr 2, pp 370-375 (USSR)

ABSTRACT: The author summarises his conclusions thus:
1. The diffusion mechanism of densification during sintering proposed by B. Ya. Pines and his team (Refs.1,2), cannot play any important role in the general process of densification during the period of presence in the sintered body of inter-communicating porosities. However, there is no reason to assume that the mechanism or process which brings about rapid and considerable densification during the presence of inter-communicating pores ceases completely after the formation of closed

pores.
2. The diffusion theory in the form proposed by Pines does not permit explaining high speeds of densification of metallic powders by the presence of lattice distortions and the formation of additional vacancies, since such an Card 1/3 explanation contradicts the basic assumption of this theory

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SOV/126-6-2-32/34

Discussion: On the Diffusion Theory of Sintering

consisting in the fact that the speed of flow of the substance is determined not by the total concentration of vacancies but by their concentration gradient. 3. There is reason to assume that, in the non-uniformly stressed crystalline body, the concentration of vacancies after long duration heating will be distributed in accordance with pressures at various sections of the body. The diffusion of vacancies should contribute to the establishment of such correspondence and not disturb it. It therefore follows that equalisation of the concentration of vacancies by diffusion can begin only after eliminating the non-uniform stress state. The possibility of simultaneous equalisation of the concentration of vacancies and of the pressure around sections of the surface with various curvatures without disturbing the equilibrium state is not clear; this problem requires special analysis which has not been done by the authors of the diffusion theory. 4. The theory of Frenkel' (Ref.7) which is based on the total magnitude of the concentration of vacancies and not Card 2/3 on the difference in the concentration of the vacancies,

Discussion: On the Diffusion Theory of Sintering

supplemented by the conception of "generation" of vacancies during the process of reversion is able to explain to a greater extent the phenomena observed during the process of sintering of real ceramic metals. However, this theory does not reveal the atomic mechanism of the process and, therefore, such an explanation of the kinetics of the densification is of semi-phenomenological character.

It is at present not possible to clarify fully the influence of lattice distortions on the speed of densification during sintering, since the atomic mechanism of the flow of metal under low load values has not been sufficiently clarified.

There are 13 references, 10 of which are Soviet, 3 English. SUBMITTED: November 20, 1956

Card 3/3 1. Sintering 2. Diffusion--Theory

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SOV/137-58-10-20812

Z.V.

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 10, p 66 (USSR)

AUTHOR:

Ivensen, V.A.

TITLE:

A New Grade of Hard Alloy, VK6M, for Machining Stainless Steel and Hard Chilled Pig Iron [Novaya marka tverdogo splava VK6M dlya obrabotki nerzhaveyushchey stali i tverdogo

(otbelennogo) chuguna |

PERIODICAL:

Prom.-ekon. byul. Sov. nar. kh-va Sverdl. ekon. adm. r-na,

1958, Nr 4, p 75

ABSTRACT:

VK6M, a new grade of hard alloy, has been developed by VNIITS for machining various stainless steels and hard chilled pig irons. VK6M differs significantly from the hard alloys VK6 and VK8 by its low porosity (< 0.05%), its extremely fine granular structure (most of the grains are under one micron) and the uniform distribution of Co. Thanks to these properties, VK6M alloy is of high strength and resistance to wear.

1. Tool steel--Development 2. Tool steel--Materials

--Stainless steel--Machining

Card 1/1

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•	PHASE I BOOK EXPLOITATION SO	V/5581		-	
	Moscow. Dom nauchno-tekhnicheskoy propagandy.				
	Vysokoproizvoditel nyy rezhushchiy instrument [sbornil Productive Cutting Tools; Collection of Articles) Mashgiz, 1961. 354 p. Errata slip inserted. 10,0 printed.	NOGCON I			
	Sponsoring Agency: Obshchestvo po rasprostraneniyu po i nauchnykh znaniy RSFSR. Moskovskiy dom nauchno- propagandy imeni F. E. Dzerzhinskogo.	oliticheskikh tekhnicheskoy	•		
	Ed. (Title page): N. S. Degtyarenko, Candidate of Tec Sciences; Ed. of Publishing House: I. I. Lesniches Ed.: Z. I. Chernova; Managing Ed. for Literature Treatment of Metals and Machine-Tool Making: V. V Engineer.	on Cold			•
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COVERAGE: The collection contains information on the following:  new brands of high-speed steels and hard alloys; designs of built-up tools and tools for the machining of holes; tools for machining heat-resisting and light-metal alloys and plastics; tools for unit-head machines and automatic production lines; and methods for the sharpening and maintenance of carbide- tipped tools. No personalities are mentioned. There are 56 references, mostly Soviet. References accompany some of the articles.	:	Service of the servic	K (), A designation of the second sec	
TABLE OF CONTENTS:  Foreword  I. NEW BRANDS OF HIGH-SPEED STEELS AND HEAD ALLOYS	3			•
Geller, Yu. A. [Doctor of Technical Sciences, Professor]. Highly Productive High-Speed Steels	7			
Card-2/6			A TANKEN OF THE STREET	
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Highly Productive Cutting Tools (Cont.) SOV/5581	
Ryvkin, G. M. Tools for Automatic Production	222
V. TECHNIQUE OF MAKING AND BRAZING CARBIDE TOOLS	
Ivensen, V. A. Production of Small-Size Shaped Carbide Tools From Plasticized Blanks	265
Anan'ina, G. S. [Engineer]. Making Small-Size Carbide Milling Cutters	273
Budnikov, N. Ye. Rational Methods in Brazing Carbide-Tipped Tools	281
VI, TOOL-SHARPENING METHODS	
Degtyarenko, N. S. [Candidate of Technical Sciences]. Sharpening of Cutting Tools [Made] of High-Speed Steel	303
Card 5/6	

APPROVED FOR RELEASE: 03/20/2001 CIA-RDP86-00513R000619320002-8"

IVENSEN, V.A.

Strength of ceramic-metal hard alloys. Porosh. met. 1
no.5:26-32 S-0 '61. (MIRA 15:6)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh
splavov. (Geramic metals—Testing)

APPROVED FOR RELEASE: 03/20/2001 CIA-RDP86-00513R000619320002-8"

S/125/61/012/002/018/019 18.9500 26566 E032/E514 Ivensen, V.A., Koval'skiy, A.Ye, Semenovskaya, S.V. AUTHORS: and Eyduk, O.N. On the anisotropy of the elastic properties of TITLE: tungsten monocarbide PERIODICAL: Fizika metallov i metallovedeniye, 1961, Vol.12, No.2, pp.299-300 In view of the difficulties in the production of TEXT: single crystals of tungsten monocarbide and the determination of their properties, the present authors have investigated the anisotropy of its elastic properties using a single crystal of WC-Co (10 wt.% cobalt). It is known that reversible (i.e.elastic) thermal stresses occur in two-phase alloys as a result of differences in the thermal expansion coefficients of the two phases. In the present work the absolute magnitude of the stresses was measured using the  ${\it yPC-50}$  (URS-50) diffractometer with Co  $K_{\alpha}$  radiation. The latter radiation was employed in with Co KB radiation. order to exclude effects associated with the doublet structure of The displacement of the "centre of gravity" of the lines K<sub>ala2</sub>. Card 1/3

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On the anisotropy of the elastic ...

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due to the specimen, relative to the lines due to a free specimen of tungsten carbide, was measured. In addition to this shift, a determination was made of the "structural" width of the  $\beta$  line due to the nonuniformity of the thermal stresses. The width of the lines obtained after the removal of the cobalt phase (by means of hydrochloric acid) was subtracted from the total width, since the removal of cobalt removes the thermal stresses. The subtraction was carried out with the aid of a linear formula. It was found that as the direction of the crystallographic plane approaches the c-axis, the elastic modulus increases. For example, the elastic modulus along the c-axis is greater than that along the a-axis by a factor of 1.5. Assuming a three-dimensional stress state, it is concluded that the tungsten carbide lattice in the alloy is compressed, which is in agreement with all the published models describing thermal stresses in the two-phase system (Ref. 2: G. P. Zaytsev, FMM, 1956, 2, No.3, 494; Ref. 3: W. Spath: Metall. 1958, No.10; Stahlbau, 1958, 24, No.3; Ref.5: J. Gurland, J. Trans. ASM., 1958, 50, 1063). The cobalt lattice, on the other hand, should be in a stretched state. It is pointed out, however, that Card 2/3

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the anisotropy may also be due to the fact that the thermal expansion coefficient is not the same in all directions. However, according to A. M. Belikov (Ref.10: Dissertation, MIS, 1958) the expansion coefficient along the a and c axes is in fact practically the same  $(3.84 \times 10^{-6} \text{ and } 3.90 \times 10^{-6})$ . There are 1 table and 10 references: 7 Soviet and 3 non-Soviet.

ASSOCIATION:

Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov (All Union Scientific Research

Institute for Hard Alloys)

SUBMITTED:

March 11, 1961

Card 3/3

TRET'YAKOV, Vsevolod Ivanovich. Prinimali uchastiye: CHAPCROVA, I.N., kand. tekhn. nauk; KOVAL'SKIY, A.Ye., kand. khim. nauk; BARANOV, A.I., inzh.; MEYERSON, G.A., prof., doktor tekhn. nauk, retsenzent; IVENSEN, V.A., kand. tekhn. nauk, retsenzent; BABICH, M.N., inzh., retsenzent; OL'KHOV, I.I., red.; MISHARINA, K.D., red. izd-va; DOBUZHINSKAYA, L.V., tekhn. red.

[Ceramic-metal hard alloys; physicochemical principles of their production, properties and fields of use] Metallokeramicheskie tverdye splavy; fiziko-khimicheskie osnovy proizvodstva, svoistva i oblasti primeneniia. Moskva, Gos.nauchno-tekhn.izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1962. 592 p. (MIRA 15:1)

(Ceramic metals)

IVENSEN, V.A.; KOVAL'SKIY, A.Ye.

Dependence of the electric resistance of a tungsten carbide-cobalt alloy on its structure. Fiz. met. i metalloyed. 13 no.5:793-794 My '62. (MIRA 15:6)

1. Vsesoyuznyy nauchno-issledovatel skiy institut tverdykh splavov.

(Tungsten-Cobalt alloys-Electric properties)

ACCESSION NR: AP4015266

5/0226/64/000/001/0056/0064

AUTHORS: Ivensen, V. A.; Eyduk, O. N.

TITLE: The structure of two-phase solid cermet alloys

SOURCE: Poroshkovaya matallurgiya, no. 1, 1964, 56-64

TOPIC TAGS: WC Co alloy, carbide phase structure, cobalt phase structure, binary cermet alloy, cermet, Co phase microscopic analysis, WC phase microscopic analysis

ABSTRACT: A discussion concerning the structure of WC-Co alloys is presented. It starts with a short review of the opinions expressed by other authors and a criticism of their conclusions. According to previous investigations, the analyses made with electron microscope showed that the carbide phase appeared to be continuous while the cobalt phase was concentrated in the inclusions, seemingly isolated from each other. However, this isolation was observed only in the polished sections. On the other hand, the fact that cobalt was removed from the alloy by the action of hydrochloric acid pointed to the existence of connections between the isolated cobalt areas. The authors believe that the degree of carbide grain coalescence depends on the differences in the technical process involved, and they claim that the cobalt "interlayers" between the carbide grains Cord 1/2

ACCESSION NR: APLOLS266

affect the physical nature of the material. It is concluded that the degree of carbide grain coalescence should be regarded as a very important structural characteristic of the alloy studied and that it should be accounted for (together with such other structural characteristics as the grain size, etc) in determining the physical properties of the WC-Co alloy. Orig. art. has: 7 photographs.

ASSOCIATION: Vsesoyuznywy nauchno-issledovatel skiy institut twerdywkh splavov, Moscow (All-Union Scientific Research Institute of Hard Alloys)

SUBMITTED: 13Feb64

DATE ACQ: 12Mar64

ENCL: 00

SUB CODE: ML

NO REF SOV: 009

OTHER: 008

Card 2/2

ACCESSION NR: AP4044910

8/0226/64/000/004/0043/0057

AUTHOR: Ivensen, V.A., Eyduk, O.N., Pivovarov, L.Kh.

TITLE: Some regularities in the deformation of sintered hard alloys of WC-Co

SOURCE: Poroshkovaya metallurgiya, no. 4, 1964, 43-57

TOPIC TAGS: sintered alloy, powder alloy, tungsten carbide, hard alloy, cobalt alloy, tungsten carbide alloy, alloy deformation, plastic deformation, alloy structure, yield point

ABSTRACT: It has recently been established that there is no direct relationship between the bending strength of a hard alloy and its notch toughness, and this fact has attracted interest to phenomena connected with the deformation of hard alloys. However, the relative deformations of the cobalt and the carbide phases and their separate roles in the total deformation process have not yet been clarified. In order to fill this gap, the present authors investigated the hard alloy WC-Co with respect to plastic deformation and its dependence on the composition (6-50% Co) and structure (fine grain and coarse grain). Prismatic test specimens (10x10x20 mm) of the hard alloy were deformed under the influence of gradually increasing uniaxial compressive loads. The residual

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#### ACCESSION NR: AP4044910

card 2/3

deformation was measured by an optimeter and the yield point was determined from logarithmic stress-strain curves, corresponding to a permanent strain of 0.1%. The lateral faces of the specimens were ground and polished before the tests, and some of the specimens were subjected to X-ray investigations before and after deformation. Such specimens were annealed at 800C before deformation to remove the strainhardening effect produced by the grinding. The width of the radiospectrographic lines was measured by the ionization method. Grain size and angle of disorientation were computed from the number and size of the reflexes obtained photographically. These studies revealed plastic deformation of the tungsten carbide grains, as indicated by numerous bands of slippage appearing on the surface of the grains after deformation, as well as by an increase in the number of reflexes on the X-ray picture. The yield point of the hard alloy was found to be directly proportional to the relative value of the contact surface of the tungsten carbide grains. The resistance to deformation of the alloy in the initial stages is determined mainly by the resistance to deformation of the carbide skeleton. It is only after further deformation that the resistance to deformation of the strain-hardened cobalt phase is manifested. The mechanism of deformation of the carbide skeleton of the alloy does not differ in principle from that of a polycrystalline

#### "APPROVED FOR RELEASE: 03/20/2001

ACCESSION NR: AP4044910

metal. Orig. art. has: 4 graphs, 15 photomicrographs and 6 tables.

ASSOCIATION: Vsesoyuzny\*y nauchno-issledovatel'skiy institut tverdy\*kh splavov (All-Union Scientific Research Institute of Hard Alloys)

SUBMITTED: 15Aug63

ENCL: 00

SUB CODE: MM

NO REF SOV: 003

OTHER: 006

3/3 Card

IVENSEN, V.A.; EYDUK, O.N.; FIVOVAROV, L.Kh.

Regularities of the deformation of We-Co ceramic metal hard alloys.

Porosh.met. & no.4:43-57 J1-Ag '64. (MIRA 18:8)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov.

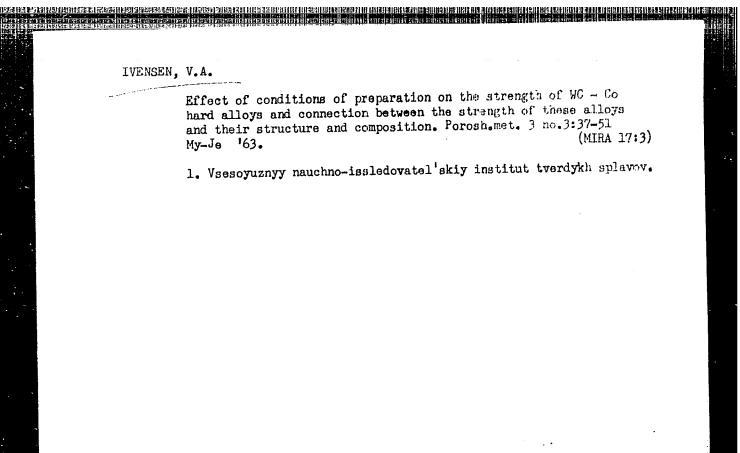
IVENSEN, V.A.; GOL'DBERG, Z.A.; EYDUK, O.N.; FAL'KCVSKIY, V.A.

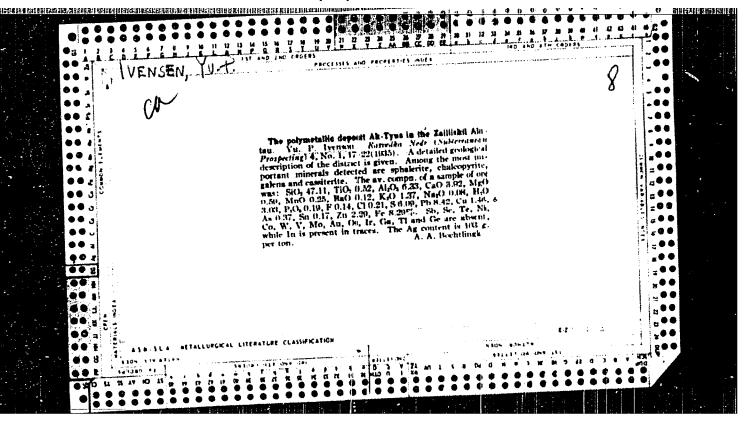
Resistance of a hard alloy to fracture under shock loads.
Porosh.met. 5 no.12:69-72 D '65. (MIRA 19:1)

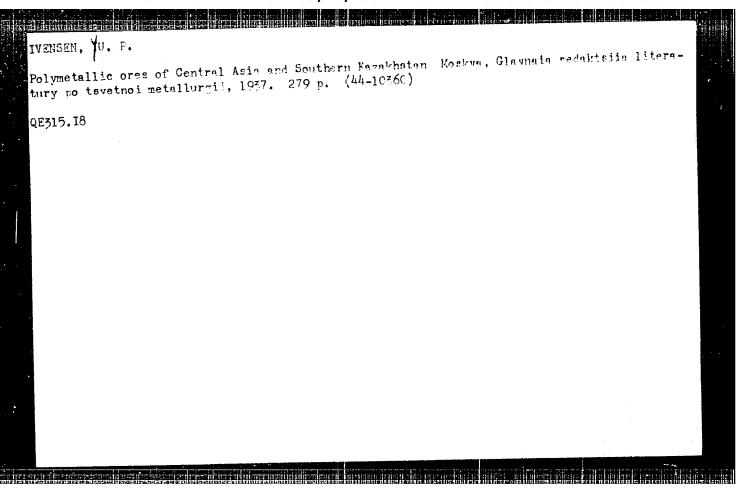
1. Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov. Submitted Pebruary 13, 1965.

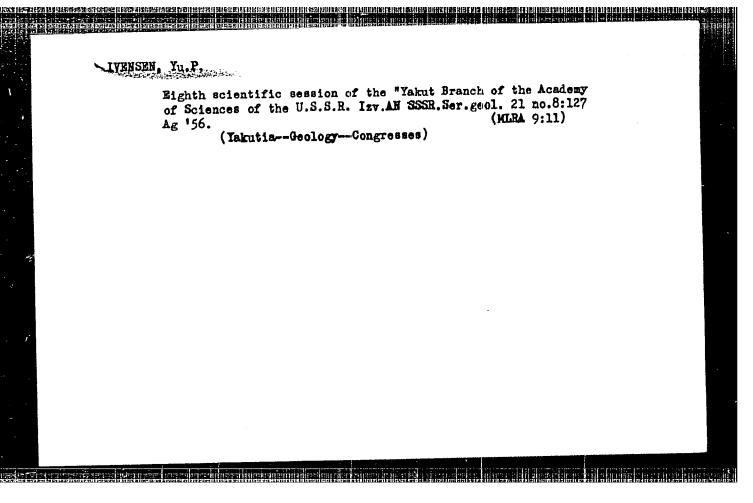
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SOURCE CODE, HR/0224	/65/000/012/0069/0072
AUTHOR: Ivenson V	03/000/012/0069/0072
V. A. Ivensen, V. A.; Gol'dberg, Z. A.; Evduk	35
AUTHOR: Ivensen, V. A.; Gol'dberg, Z. A.; Eyduk,	O. H. Fal'kovakta B
ODC.	
All-Union Scientific Research	
ORG: All-Union Scientific Research Institute of I uznyy nauchno-issledovatel skiy institut tverdykh	ard Allona (v.
mrm- unstitut tverdykh	#Dlavou)
TITLE: Resistance of a hand	
TITLE: Resistance of a hard alloy to failure under SOURCE: Poroshkovene	
SOURCE: Poroshkovaya metallurgiya, no. 12, 1965,	Tubade Toada
metallurgiya, no. 12. 1969	排2.基础 法国国际公司重新
TOPIC TAGS: places	
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TOPIC TAGS: plastic deformation, mechanical shock data analysis, tungsten contains.	resistance, specific
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ABSTRACT. The	
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that despite the relatively low value of plastic de This was corroborated to the efficiency of the	ard alloy on its
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latter has a great effect on the efficiency of the of a very coarse-prained experimental data character	hard-alloy load
This was corroborated by experimental data characters of a very coarse-grained and a medium-grained alloy much greater than there are efficiency of the coarse-	wizing the affice
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11-8-13/14 Ivensen, Yu.P. AUTHOR: Letter to the Editorial Office of the Magazine "Izvestiya TITLE: AN SSSR, Seriya Geologicheskaya" (V redaktsiyu zhurnala "Izvestiya AN SSSR, Seriya Geologicheskaya") Izvestiya Akademii Nauk SSSR, Seriya Geologicheskaya, 1957, PERIODICAL: # 8, p 111 (USSR) The author refers to his paper published in # 3, 1957, this ABSTRACT: magazine, whose reference list omitted G.G. Rodionov's paper on "the mechanism of shaping pegmatite veins", published in 1956. The author confirms Rodionov's priority and corrects his omission by publishing the present letter. 28 May, 1957 SUBMITTED: Library of Congress AVAILABLE: Card 1/1

Defense of Dissertations. January - July 1957.

30-12-36/45

Section

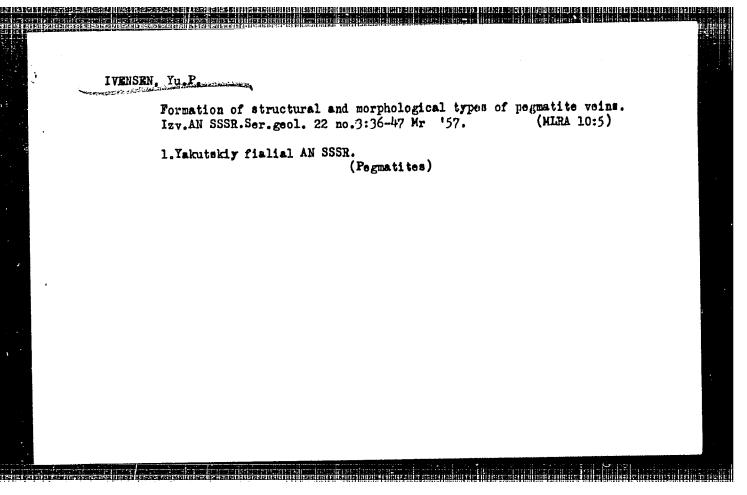
of Geological-Geographical Sciences (Vest. AN SSSR, 1957, V.27, No.12 p 113-115)

> sostava i mekhanicheskikh svoystv mermlykh gruntov ot temperatury i davleniya). Application for the degree of Candidate of Geographical Sciences: N. G. Bobrov - The peculiar features of the mass of rocks frozen for many years and their accompanying formations in the Southern Koryak district and on Northern Kamchatka (Osobennosti tolshchi mnogoletnemerzlykh gornykh porod i soputstvuyushchikh im obrazovaniy v Yuzhno-Koryakskoy strane i na Severncy Kamchatke).

At the Instate for the Geology of Ore Deposits, Petrography, Mineralogy, and Geochemistry (Institut geologii rudnykh mestorozhdeniy, petrografii, mineralogii i geokhimii). Applications for the degree of Doctor of Geological-Mineralogical Sciences: Yu. P. Ivensen - The forming of granite pegmatites in connection with the development of geological structure. (Stanovleniye granitnykh pegmatitov v svyazi s razvitiyem geologicheskoy struktury). A. S. Povarennykh - crystallochemical bases of the modern text book of Mineralogy (Kristallokhimicheskive osnovy sovremennogo

Card 3/4

IV	TENSEN, Yu.P.	
	Studying the genesis of granitic pegmatites. Izv.vost.fil.AN SSER no.7:15-21 '57. (MIRA 10:10)	
	1. Yakutskiy filial AN SSSR. (Pegmatites)	



FISHMAN, M.V.; SIMAKOV, G.V.; GOLDIN, B.A.; IVENSEN, Yu.F., oty.red.;
MOROZOVA, A., otv.za vypusk; TSIVUMIN, T., tekhn.red.

[Granitoid intrusions in the upper Bol'shoy Patok, Malyy Patok, and Torgovaya Valleys (Polar Urals) and the related mineralization]
Granitoidnye intruzii verkhovii Bol'shogo Patoka, Malogo Patoka
i Torgovoi (fripoliarnyi Ural) i sylazannoe u nimi orudenenie.
Syktyvkar, Komi knizhnoe izd-vo, 1960. 99 p. (Akademiia nauk
SSSR. Komi filtal, Syktyvkar. Institut geologii. Trudy, no.1).

(Ural Mountains--Rocks, Igneous)
(Ural Mountains--Ore deposits)

DEVYATOVA, Eleonora Ivanovna; MARKOV, K.K., doktor googr. namk, prof., otv. red.; IVENSEN, Yu.P.., doktor geol.-mineral. nauk, otv. red.; SHENGER, I.A., red. izd-va; ZENDEL', M. Te., tekhn. red. [Stratigraphy of Quaternary sediments and paleogeography of the Quaternary period of the Onega basin] Stratigrafiia chetvertichnykh otlozhenii i paleogeografiia chetvertidanogo perioda v basseine reki Onegi. Moskva, Izd-vo Akad. nauk SSSR, 1961. 88 p. (MIRA 14:8) (Onega Valley-Paleogeography) (Onega Valley-Geology, Stratigraphic)

CHALYSHEV, Vasiliy Ivanovich; <u>IVENSEN</u>, Yu.P., doktor geologo-miner. nauk, otv. red.; TSVETKOV, N.V., red. izd-va; BOCHEVER, V.T., tekhn. red.

[Stratigraphy and lithology of Permian and Triassic Lagornal and terrestrial deposits in central Pechora] Stratigrafiia i litologiia lagunno-kontinental nykh otlozhenii permi i triasa Srednei Pechory.

Moskva, Izd-vo Akad.nauk SSSR, 1961. 102 p. (MIRA 14:6)

(Pechora Valley—Geology, Stratigraphic)

(Pechora Valley—Petrology)

IVENSEN, Yu.P., doktor geol.-miner. nauk, otv. red.; KULIKOV, M.V., red. izd-va; ZENDEL', M.Ye., tekhn. red.

[Materials on the geology and petrography of the Timan Ridge and Kanin Peninsula] Materialy po geologii i petrografii Timana i poluostrova Kanin. Moskva, Izd-vo Akad. nauk SSSR, 1961. 146 p. (MIRA 14:11)

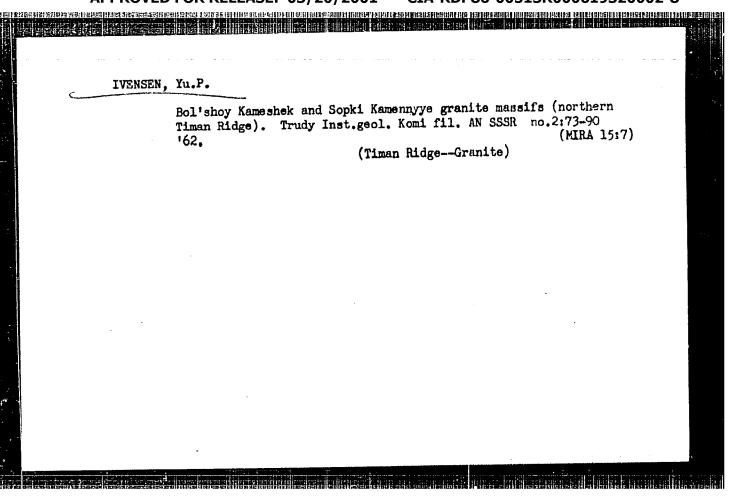
1. Akademiya nauk SSSR. Komi filial, Syktyvkar. Institut geologii. (Timan Ridge—Geology)

VIKHERT, A.V.; VOZIN, V.F.; IVENSEN, Yu.P.; KASHIRTSEV, A.S.; PROSHCHENKO, Ye.G.; CHEPIKOVA, I.M., red.izd-va; GUS'KOVA, O.M., tekhn.red.; MAKAGONOVA, I.A., tekhn.red.

[Geology and ore potential of the western Verkhoyansk Range]
Geologicheskoe stroenie i rudonosnost' Zapadnogo Verkhoianiia.

Moskva, Izd-vo Akad.nauk SSSR, 1961. 210 p. (Akademia nauk SSSR. IAkutski fillal, Yakutsk. Trudy, no.5). (MIRA 15:2)
(Verkhoyansk Range---Oer deposits)

(Verkhoyansk Range---Ore deposits)



PUSTOVALOV, L.V., otv. red.; AL'TGAUZEN, M.N., doktor geol.-min. nauk, red.; DOLGOFOLOV, N.N., red.; IVENSEN, Yu.P.. doktor geol.-min. nauk, red.; VLASOV, K.A., doktor geol.-min. nauk, red.; FOZHARITSKIY, K.L., doktor geol.-min, nauk, red.; SERDYUCHENKO, D.P., doktor geol.-min. nauk, red.

[Metals in sedimentary formations; ferrous metals, non-ferrous light metals] Metally v osadochnykh tolshchakh; chernye metally, tsvetnye legkie metally. Moskva, Izd-vo "Nauka," 1964. 443 p. (MIRA 17:8)

1. Akademiva nauk SSSR. Laboratoriya osadochnykh poleznykh iskopayemykh. 2. Chlen-korrespondent AN SSSR (for Fustovalov, Vlasov).

IVERSEAVA, A. W.

"Critical Review of Foreign Post-War Pediatric Literature," Pediatrics, No. 3, 1949, Moscow

IVENSKAYA, A-M.

FRIGINA, S. IA., IVENSKAIA, A. M.

Combined tuberculosis and diphtheris vaccination, Probl. Tuberk., Hoskva No. 6, Nov.-Dec. 50. p. 42-4

1. Of the Pediatric Clinic of the Academy of Medical Sciences (Tuberculosis Division) (Scientific Director—Prof. 1. V. Tsimbler) and of the Institute for the Control of Bacterial Preparations imeni Tarasevich (Scientific Director—P. F. Zdredovskiy, Active Hember of the Academy of Medical Sciences).

CLML 20, 3, March 1951.

IVENSKAYA. A.M.; NOSKACHEVA, K. A.

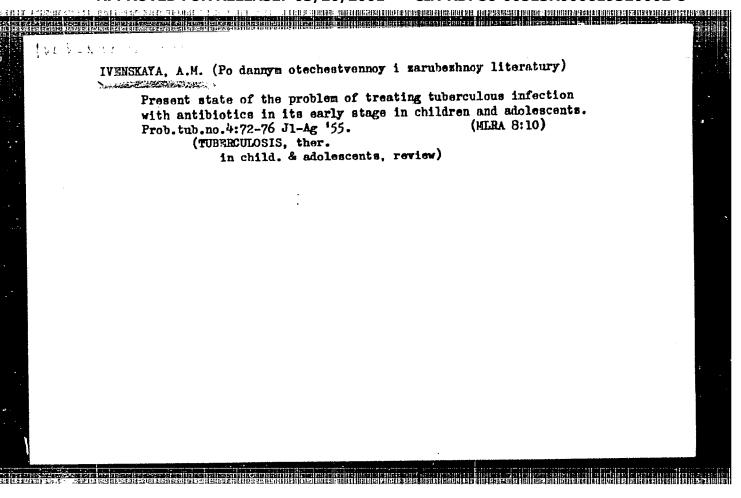
Streptomycin therapy of general miliary tuberculosis in children. Sovet. med. no.10:13-17 Oct 1951. (CIML 21:1)

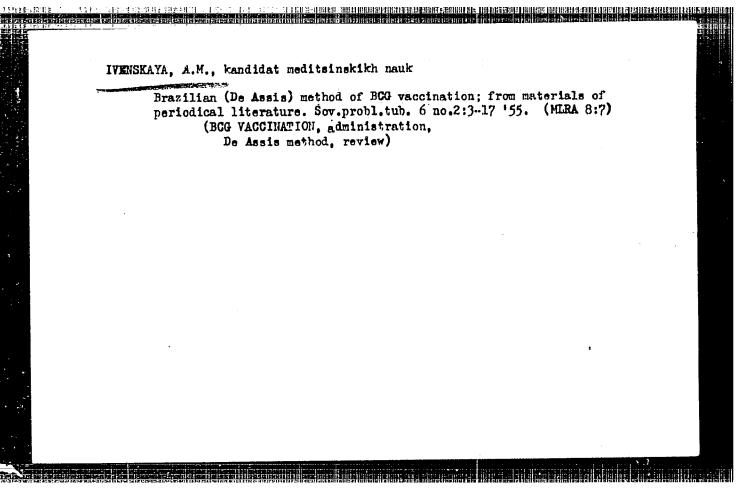
1. Candidate Medical Sciences Ivenskaya; Candidate MedicalSciences Moskacheva. 2. Of the Clinic for Tuberculosis (Head -- Prof. I. V. Tsimbler), Institute of Pediatrics of the Academy of Medical Sciences USSR (Director -- Honored Worker in Science Prof. G. N. Speranskiy).

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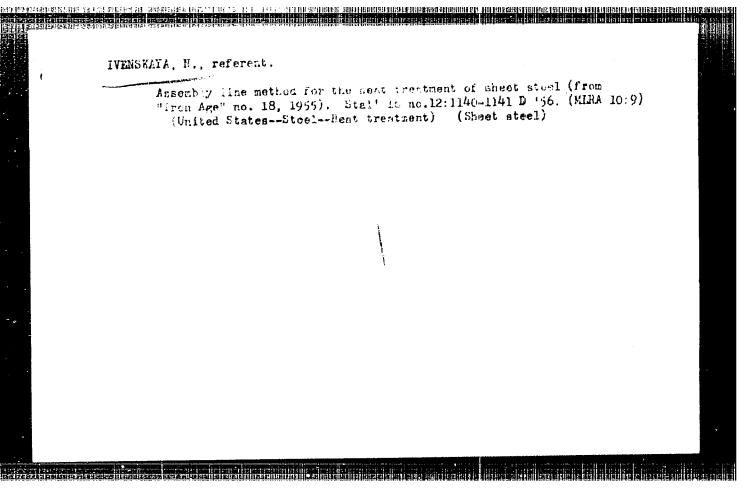
IVENSKAYA, A.M., kandidat meditainakith neuk IVENSKAYA, A.M., kandidat meditsinskikh nauk. Early prophylactic therapy for primary infection with untibiotics. Sovr.probl.tub. 5 no.5:3-7 '54. (MIRA 8:1) (Antibiotics) (Tuberculosis)





ARUTYUNOV, V.Ya., prof.; BERKOVICH, I.M., doktor med.nauk; BUNIN, K.V., prof. VELIKORETSKIY, A.N., prof.; GAMBURG, R.L., doktor med.nauk; GIASKO, N.M.; ZVYAGINTSEVA, S.G., doktor med.nauk; LYMMSKAYA-PAVIOVA, Z.A., prof. nauk; KALUGINA, A.N., kand.med.nauk; KAMINSKAYA-PAVIOVA, Z.A., prof. KVATER, Ye.I., prof.; KOLEN'KO, A.B., prof.; KOSSYURA, M.B., kand. med.nauk; KRAVETS, E.M., doktor med.nauk; KRISTMAN, V.I., kand.med.nauk; KRUZHKOV, V.A., dotsent; LIKHACHEV, A.G., prof.; LUKOMSKIY, I.G., prof.; MASHKOVSKIY, M.D., prof.; ROZENTAL', A.S., prof.; SERRYSKIY, M.Ya. [deceased], prof.; TURETSKIY, M.Ya., kand.med.nauk; KHESIN, Ye.Ye., dotsent; EMDINA, Kh.L., kand.med.nauk; SHABANOV, A.H., prof.; red.; BOMDAR', Z.A., red.; ZAKHAROVA, A.I., tekhn.red.

[Medical handbook for feldshers] Meditsinskii spravochnik dlia fel'dsherov. Izd. 6-oe, perer. i dop. Moskva, Gos. izd-vo med. lit-ry, 1957. 899 p. (MIRA 10:12) (MEDICINN--HANDBOOKS, MANUALS, ETC.)



SOV/137-57-1-1145

Translation from: Referativnyy zhurnal. Metallurgiya, 1957, Nr 1, p148 (USSR)

AUTHOR: Ivenskaya, N. D.

TITLE: Application of Metallic Coatings in a Gaseous Medium (Naneseniye

metallicheskikh pokrytiy v gazoobraznoy srede)

PERIODICAL: Tekhnol. transp. mashinostroyeniya, 1956, Nr 3, pp 70-75

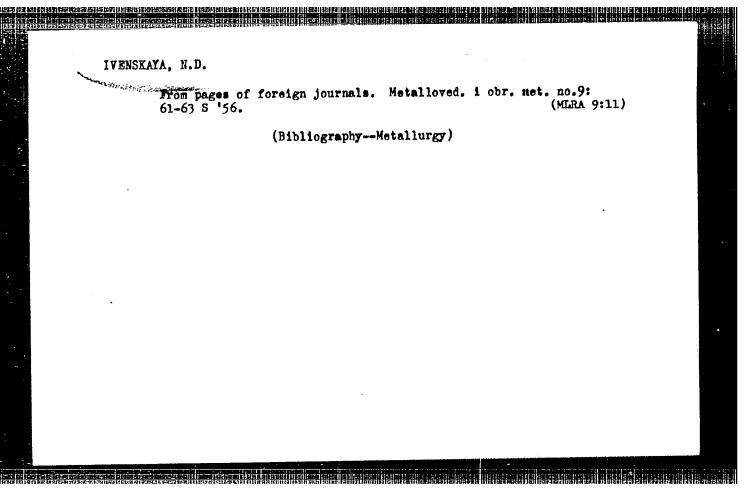
ABSTRACT: A survey of "Steel" magazine for 1953 and 1955 on the plating (P) of articles with metals obtained from a gaseous phase (GP). A description is given of the chemism of the process, the equipment used, and the properties of the P obtained from a GP. A comparison of the processes of gaseous and galvanic P and the application of gaseous P are adduced. The following three composite tables are adduced: 1) Properties of carbonyls of different metals; 2) ductility and resistance to oxidation of various P deposited from

GP of metals as well as carbides, nitrides, borides, silicides,

and oxides; 3) the purposes of specific P.

M. Z.

Card 1/1



SOV-129-58-6-17/17

AUTHOR: Ivenskaya, N. D.

TITLE: Non-Russian Literature on Equipment for Heat Treatment and High Temperature Alloys (Oborudovaniye dlya termicheskoy obrabotki)

PERIODICAL: Metallovedeniye i Obrabotka Metallov, 1958, Nr 6, pp 63-64 (USSR)

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ABSTRACT: List containing 7 references on equipment for heat treatment and 11 references on high temperature alloys.

1. Literature - USSR 2. Alloys 3. Induction heating - Equipment

Card 1/1

USCOMM-DC-55498

28(4)
AUTHOR:

Ivenckaya, N. D., Abstracter

Abstract. Improvement in the Methods of Producing
Mirror-finished Metallographical Samples (Metall Progress, X,
1958, Vol 78, Nr 5, p 145)

PERIODICAL:

Zavodskaya laboratoriya: 1959, Vol 25, Nr 9, pp 1099-1100 (USSR)

Abstract:

This is an abstract from the afore-mentioned article, published
in the periodical mentioned in the subtitle, including a diagram
of the instrument described (Fig). There is 1 figure.

DONSKOY, Al.V., doktor tekhn. nauk, prof.; DONSKOY, An.V.;
DRESVIN, S.V.; IVENSKIY, C.V.; KUKHTIN, A.M.; LETBIN,
Yu.V.; MONDRUS, D.B.; SOLOMAKHIN, I.M.; FRUMKIN, A.A.;
BALASHOV, V.A., retsenzent

[High-frequency electrothermy; a handbook] Vysokochastotnaia elektrotermiia; spravochnik. Moskva, Mashinostroenie,
1965. 564 p. (MINA 18:6)

DONSKOY, Aleksandr Vasil'yevich; IVENSKIY, Grigoriy Vasil'yevich;
FOSSE, A.V., kand. tekhn. nauk, retsenzent; MCMDRUS, D.B.,
kand. tekhn. nauk, retsenzent; S ORODINOV, V.V., red.

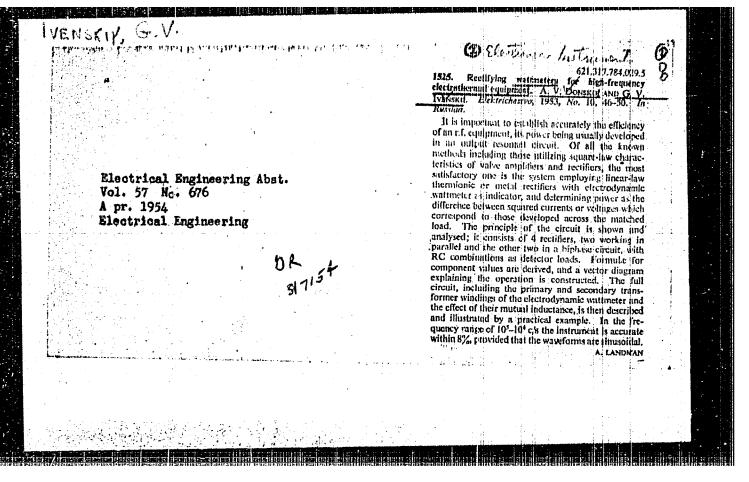
[Electrothermal systems with electronic converters with increased frequency] Elektrotermichaskie ustanovki s ionnymi
preobrazovateliami povyshennoi chastoty. Moskva, Izd-vo
"Energiia," 1964. 209 p. (MIRA 17:6)

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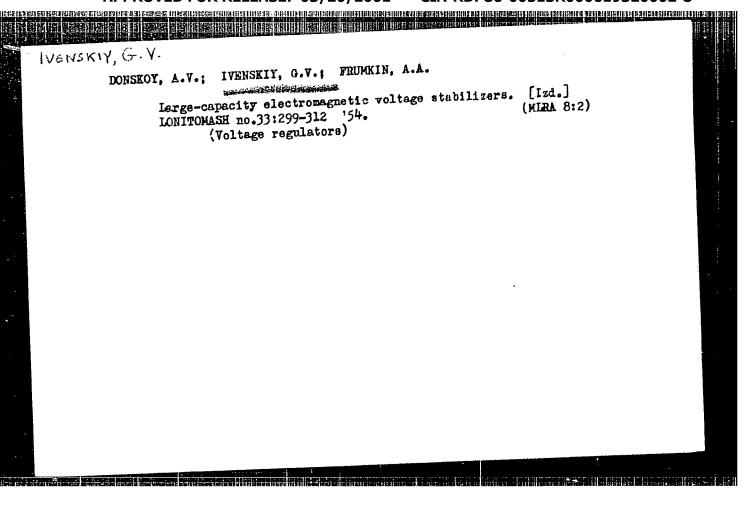
#### CIA-RDP86-00513R000619320002-8



SHLYAPOSHNIKOV, Boris Moiseyevich, professor; IVENSKIY, G.V., redaktor;
VOR(NETSKAYA, L.V., tekhnicheskiy redaktor; internalisinistic

[Laboratory manual on electronic and ionic devices] hakovodatvo k laboratorii elektronnykh i ionnykh ustroistv. Moskva, Oos. energ. izd-vo, 1954, 299 p. (MLEA 7:11)

(Zlectronics)



DONSKOY, Afeksandr Vasil'yevich, doktor tekhn.nauk; IVENSKIY, Grigoriy
Vasil'yevich, inzhener; ACHKINADZE, Sh.D., red.; YREGER, D.P., tekhn.red.

[Stabilized anode rectifier for electrothermal equipment; practices of "Sevzappromelektropich"" and the M.I.Kalinin Polytechnic Institute in Leningrad] Stabilizirovannyi anodnyi vypriamitel' dlia elektrotermicheskik ustanovok; iz opyta "Sevzappromelektropech" i LPI imeni M.I.Kalinina. Leningrad, 1956. 14 p. (Leningradskii dom nauchno-tekhnicheskoi propagandy. Informatsionno-tekhnicheskii listok, no.19. Elektricheskie netody obrabotki metallov) (MIRA 10:12)

(Electric current rectifiers)

SOV/112-59-4-7852 Translation from: Referativnyy zhurnal. Elektrotekhnika, 1959, Nr 4, p 204 [USSR] TITLE: Investigation of a Grid-Controlled Rectifier Unit That Supplies the PERIODICAL: V sh.: Prom. primeneniye tokov vysokov chastoty. Riga, 1957, AUTHOR: Ivenskiy, G. V. ABSTRACT: A rectifier unit intended for supplying & high-frequency electrothermal circuit and with a grid-installation and designed with a 3-phase bridge circuit and with a gridinstallation and designed with a 3-phase bridge circuit and with a shape controlled cathode group is analyzed for the cause of presence and absence controlled cathode group is analyzed for the cause of presence and absence controlled cathode group is analyzed for the cause of presence and absence controlled cathode group is analyzed for the cause of presence and absence controlled cathode group is analyzed for the cause of presence and absence and absence controlled cathode group is analyzed for the cause of presence and absence controlled cathode group is analyzed for the cause of presence and absence cathode group is analyzed for the cause of presence and absence cathode group is analyzed for the cause of presence and absence cathode group is analyzed for the cause of presence and absence cathode group is analyzed for the cause of presence and absence cathode group is analyzed for the cause of presence and absence cathode group is analyzed for the cause of presence and absence cathode group is analyzed for the cause of presence and analyzed for the cause of the caus installation and designed with a 3-phase bridge circuit and with a gridcontrolled cathode group is analyzed for the Cases of presence and absence of a controlled cathode group is analyzed for the cases of the transformer winding device in the neutral and that the transformer winding device in the neutral and that the transformer winding device in the neutral and that the transformer winding device in the neutral and that the transformer winding the neutral and the period of the case of the c controlled cathode group is analyzed for the cases of presence and absence of rectifying device in the neutral. It is assumed that the transformer estimates of a graph of registance is zero and the load is nursely registance. On the basis of a graph of registance is zero and the load is nursely registance. rectifying device in the neutral. It is assumed that the transformer winding On the basis of a graphoresistance is zero and the load is Purely restifier current and voltage curves analytical solution of a set of sevations. resistance is zero and the load is purely resistive. On the basis of a grapho-analytical solution of a set of equations, rectifier current and voltage curves analytical solution of a set of equations, rectifier current and the control characteristics are commuted. analytical solution of a set of equations, rectifier current and voltage curves are plotted and its control characteristics are computed. The estimated data are plotted and its control characteristics are computed from a time 1 f.D7 sho how well agrees with the experimental data obtained from a time 1 f.D7 sho have are plotted and its control characteristics are computed. The estimated data obtained from a type LGPZ-60, 60-kw well agrees with the experimental data obtained from a type LGPZ-60. Card 1/2 Card

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CIA-RDP86-00513R000619320002

8(4), 9(0)

SOV/112-59-2-3698

Translation from: Referativnyy zhurnal. Elektrotekhnika. 1959, Nr 2, pp 209-210 (USSR)

AUTHOR: Donskoy, A. V., Borok, A. M., and Ivenskiy, G. V.

TITLE: Ionic Frequency Converters for Electrothermal Installations
(Ionnyye preobrazovateli chastoty dlya elektrotermicheskikh ustanovok)

PERIODICAL: V sb.: Prom. primeneniye tokov vysokoy chastoty Riga, 1957, pp 273-286

ABSTRACT. A 60-kw ionic frequency converter for electrothermal installations developed by LH imeni M. I. Kalinin is described. Its output frequency is 2,500-2.800 cps. Its scheme has an implicit DC circuit. Six TR1-15/15 thyratrons are connected on their cathode side in three groups of two and connected to the three-phase rectifying transformer; on their anode side, they are arranged in two groups of three each and connected to the terminals of a single-phase inverter transformer. A smoothing choke coil is connected

Card 1/3

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Ionic Frequency Converters for Electrothermal Installations

between the neutrals of both transformers. An oscillatory circuit formed by the furnace inductor and the phase-control capacitor serves as a load for the converter The grid-control circuit of the inverter is fed from the converter output via an RC phase shifter The self-control feature secures the following: (1) an automatic frequency control as the circuit parameters change in the course of metal heating, and (2) short-circuit protection upon collapse of inverter oscillations. However, an additional special device to open the valves for starting is required. When the power is adjusted by the phase shifter, the inverter-transformer ratio is changed and the firing-point-controlling capacitors are switched simultaneously. In the schemes with an explicit DC circuit, the rectifier grid control can be used advantageously. Experimental regulating and load characteristics of the converter are presented. It is pointed out that in schemes with higher frequencies, it is expedient to prolong the recovery time for the valves. Another solution is to use a converter with a

Card 2/3

SOV/112-59-2-3698

Ionic Frequency Converters for Electrothermal Installations

triple output frequency; its briefly presented scheme is a combination of three single-phase inverters whose inverter-transformer secondaries are connected in open delta. Bibliography: 10 items.

V.A.L.

Card 3/3

APPROVED FOR RELEASE: 03/20/2001 CIA-RDP86-00513R000619320002-8"

I venskily,

110-12-13/19

AUTHOR: Ivenskiy, G.V., Engineer.

TITLE:

The Power Factor of Industrial Electrical Thermal Installations with Valve Generators (Koeffitsiyent moshchnosti promyshlennykh elektrotermicheskikh ustanovok s lempovymi generatorami)

PERIODICAL: Vestnik Elektropromyshlennosti, 1957, Vol.28, No.12, pp. 44 - 48 (USSR).

ABSTRACT: High-frequency industrial heating installations commonly use a three-phase thyratron circuit. To simplify the grid control circuit, only the cathode group of valves is controlled. In order to increase the power-factor at large ignition angles, use is made of a zero valve, its anode connected to the zero point of the rectifier transformer and its cathode to the common cathode of the rectifier. This article determines the power-factor of the rectifier without making assumptions about the wave- shape of the rectified current and also determines the influence of the zero valve on the power-factor. Amongst other assumptions, zero losses and magnetisation current in the rectifier transformer, and zero voltage drop in the valves are postulated. Current and voltage curves for rectifiers with and without

Cardl/2zero valves are plotted in Figs. 2 and 3. Three cases are

110-12-13/19

The Power Factor of Industrial Electrical Thermal Installations with Valve Generators.

plotted when a zero valve is used according to the value of the ignition angle and two corresponding cases are plotted for the case when there is no zero valve. Analytical expressions are derived for the active power and the power-factor. Graphs showing the relationship between the power-factor of a rectifier and the regulation factor are given in Fig. 5 for an installation type NTW-60. The experimental curves lie somewhat below the theoretical value, because of the assumptions upon which the calculation is based. The results plotted in Figs. 4 and 5 indicate that the zero valve has an appreciable influence on the power-factor of the rectifier for ignition angles greater than 70 - 80°. Further increase in the angle greatly increases the effectiveness of the zero valve. The use of the zero valve is, therefore, most advantageous when it is frequently necessary to use very low rectified voltages. There are 5 figures and 2 Slavic references.

ASSOCIATION: Leningrad Works for High-frequency Installations (Leningradskiy Zavod Vysokochastotnykh Ustanovok) SUBMITTED: November 13, 1956.

AVAILABLE:

Library of Congress.

Card 2/2

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Lucuskiy, 60

110-4-14/25

AUTHORS: Donskoy, A.V., Doctor of Technical Sciences, Professor,

Borok, A.M., Ivenskiy, G.V., and Khansuvarov, A.A., Engineers.

TITIE: A High-frequency Electro-thermal Installation of a New

Series (Vysokochastotnaya elektrotermicheskaya ustanovka

novoy serii)

PERIODICAL: Vestnik Elektropromyshlennosti, 1958, No. 4, pp. 42 - 47 (USSR).

High-frequency electro-thermal installations with valve ABSTRACT: generators for induction-heating are widely used. A massproduced equipment has lacked anode voltage stabilisation and needs careful screening to reduce radio interference. A new series of equipment has been developed that operates at a frequency of 70 kc/s, so that both the fundamental and the second harmonic are outside the standard frequency range for radio interference. This new equipment, type 5173-67, employs a stabilised anode-controller rectifier. The main technical data are given with a full-circuit diagram in Fig.1 and the main components of the circuit are described: the rated output is 60 kW. The principles of the grid control system are described. A change of the grid voltage varies the firing angle of the valve. The main advantage of the circuit is its simplicity and although the accuracy of stabilisation is less than that Cardl/2 of existing circuits, it is nevertheless adequate. The equipment

110-4-14/25 A High-frequency Electro-thermal Installation of a New Series

includes protection against short-circuit, orrload and under-voltage. A general view of the equipment is given in Fig.2. It is housed in a number of separate cubicles, whose contents are described.

A wide range of tests was made on the equipment; its characteristics are given in rig. 3. These curves show that the generator can easily be adjusted to give the best operating conditions on the most varied loads. The oscillatory power ranges from 40 - 60 kW and the efficiency of the generator valve is 72 - 78%. The power-factor depends on the ignition angles of the thyratron and ranges from 0.72 - 0.93. During the tests careful measurements were made of radio-interference with the results plotted in Fig. 4, which shows that interference is worst at light-loads but is still within the specified limits even when the cubicle doors are open.

There are 4 figures, and 3 Russian references.

ASSOCIATION:

The Leningrad Works for High-frequency Installations (Leningradskiy zavod vysokochastotnykh ustanovok)

SUBMITTED:

October 18, 1957

AVAILABLE:

Library of Congress

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8(3) AUTHORS: Donskoy, A. V., Doctor of Technical Sciences, SOV/105-59-7-10/30

Ivenskiy, G. V., Candidate of Technical Sciences, Borok, A. N.,

Engineer

Ion Frequency Converters for Induction Heating Installations TITLE:

(Ionnyys preobrazovateli chastoty dlya ustanovok induktsionnogo

nagreva)

PERIODICAL:

Elektrichestvo, 1959, Mr 7, pp 41 - 45 (USSR)

ABSTRACT:

The USSR industry at present produces large thyratrons of the TRI-15/15-type within a sufficiently short time for the re-establishment of the controllability of the grid. Investigations show that they operate with sufficient reliability in frequency converters of cycles. The wiring diagrams of these converters are 50/2500 given. As the basic wiring diagrams of similar converters have already been dealt with by the papers of references 1 and 2, the auxiliary circuits are in this case mainly investigated. Figure 1 shows the wiring of an ion frequency converter of 50/2500 cycles and

60-80 kw with a direct current term, which is described. It has been used for the melting of metal since July 1957 at the Laboratoriya elektrotermicheskikh ustanvok LEI in. Kalinina

Card 1/3

(Laboratory for Electrothermal Installations at the

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Ion Frequency Converters for Induction Heating Installations SOV/105-59-7-10/30

LPT im. Kalinina (Leningrad Polytechnic Institute imeni Kalinin). The rectifier of this converter is a three-phase single-cycle rectifier with 3 valves and one converter. The inverter is constructed as a single-phase single-cycle inverter with 2 valves and 1 converter. It is shown that an inverter for 2500 cycles embodied within the thyratron mentioned must necessarily be a single-cycle inverter. Regulation of the initial output  $\mathbf{F}_k$  is brought about by variation 1) of the capacity of the capacitor  $\mathbf{C}_k$ , 2) of the phase

shift angle  $\varphi$  between the grid- and anode voltages of the thyratrons of the inverter group, and 3) of the economy transformer coupling of the load circuit  $\mathbf{L}_k \mathbf{C}_k$  with the inverter-transformer.

The experimentally obtained characteristics of the converter corresponding to these three kinds of regulation are shown by figure 2. The disadvantage of the 1. and 2. method is the stepped regulation. Apart from the circuit shown by figure 1, where one valve group is used only for rectification and the other only for inverting the current, also ionic converters with a direct current element (Refs 1, 2) may be used in electrothermal installations. In this case the same valves are used for rectification and inversion. Such a converter, consisting of a three-phase one-cycle rectifier

Card 2/3

Ion Frequency Converters for Induction Heating Installations SOV/105-59-7-10/30

and a single-phase one-cycle inverter with 60-80 km is shown by figure 4. This inverter was investigated in the above laboratory, where it was used for a long period. The life of the thyratrons TR1-15/15 of the converter group is, as shown by experience, about 800 - 900 hours. There are 5 figures and 5 Soviet references.

ASSOCIATION:

Leningradskiy politekhnicheskiy institut im. Kalinina (Leningrad

Polytechnic Institute imeni Kalinin)

SUBMITTED:

May 16, 1958

Card 3/3

DONSKOY, Aleksandr Vasil'yevich, doktor tekhn.nauk, prof.; IVHNSKIY, Grigoriy Vasil'yevich, kand.tekhn.nauk

Autonomous parallel inverter with doubled frequency output. Izv. vys. ucheb. zav.; elektromekh. 3 no.3:125-139 '60. (MIRA 13:10)

- 1. Kafedra elektrifikatsii promyshlennykh predpriyatiy i ustanovok Leningradskogo politekhnicheskogo instituta (for Donskoy).
- 2. Vedushchiy inzhener Osobogo konstruktorskogo byuro elektrotermicheskogo oborudovaniya Leningradskogo sovnarkhoza (for Ivenskiy). (Pulse techniques (Electronics))

DONSKOY, Aleksandr Vasil'yevich; IVENSKIY, Grigoriy Vasil'yevich; MONDRUS, D.B., red.; FREGER, D.P., izd.red.; ESLOGUROVA, I.A., tekhn.red.

[New induction heating systems with ionic frequency converters]
Novye elektrotermicheskie ustanovki s ionnymi preobrazovateliami
chastoty. Leningrad, 1961. 39 p. (Leningradskii Dom nauchnotekhnicheskoi propagandy. Obmen peredovym opytom. Seriia: Elektricheskie metody obrabotki metallov, no.1).

(MIRA 14:6)

(Induction heating)

37961

S/137/62/000/005/017/150 A006/A101

1,1710

AUTHORS:

Donskoy, A. V., Ivenskiy, G. V.

TITLE:

Experimental series of electric melting units with thyratron

frequency changers for 2,500-cycle frequency

PERIODICAL:

Referativnyy zhurnal, Metallurgiya, no. 5, 1962, 51, abstract 5V304 (V sb. "Vysokochastotn. elektrotermich. ustanovki", Moscow-Leningrad,

Gosenergoizdat, 1961, 23-40)

TEXT: High efficiency, low idle-run power, and a number of other advantages distinguish positively ion frequency changers from other converter types employed in electrothermics. In 1955, the Central Designing Office for Ultrasonic and High-Frequency Units (TSKB UVU) and the Leningrad Polytechnic Institute imeni M. I. Kalinin (LPI) started investigations on the possibility of designing new medium-power (60 - 80 kw) ionic frequency changers for 2,500 cycles. The investigations have shown that domestic TP1-6/15 (TR1-6/15) and TPI-15/15 (TRI-15/15) type thyratrons can operate on the frequency indicated. Experimental semi-industrial electric melting units were developed with thyratron frequency changers with a distinctly marked d-c link. The latest unit is used at the LPI

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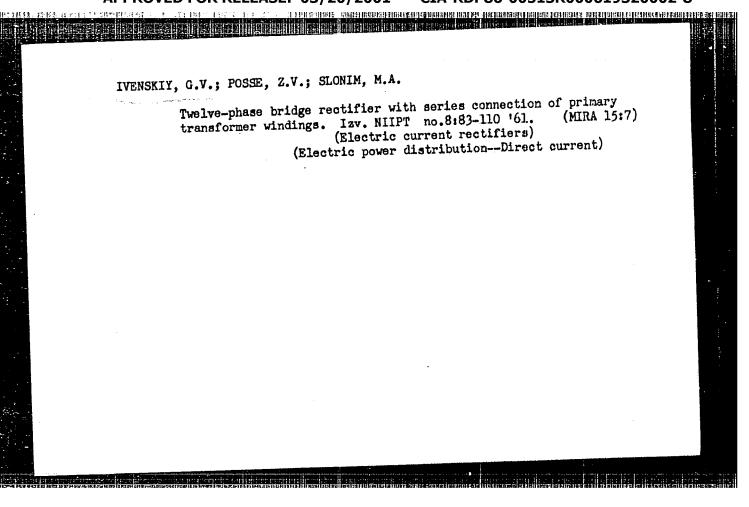
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Experimental series of electric melting ...

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from 1957 for the production of magnetic alloys. Positive results in operating this unit made it possible to develop at the TsKB UVU a series of electric melting units with TN -62 (TP-62) and TN -162 (TP-162) type thyratron frequency changers. In 1959, the Leningrad Plant of High-Frequency Units assimilated series production of TP-62 units. In 1962, a TP-162 type unit was produced and is now being tested for industrial use. Ionic frequency changers have in both units a clearly marked d-c link and consist of a three-phase single-cycle rectifier and a single-phase, single-cycle, self-excited inverter. Voltage at the rectifier output (in the inverter circuit) is 3 kv. The basic differences between TP-162 and TP-62 are: 1. In PT-62 both the rectifier and the inverter are assembled on TRI-15/15 type thyratrons. In TP-162 the rectifier is assembled on three TRI-40(15) type thyratrons and the inverter on four TRI-15/15 type thyratrons. 2. TR-162 is equipped with two melting furnaces. 3. In TP-162 there is a possibility of changing the coefficient of autotransformation on the furnace kg, to regulate the output power. Therefore the rated furnace voltage is almost twice as high as the rated voltage of the secondary winding of the inverter transformer, and amounts to 1,500 v. Unlike as in PT-62, there is no possibility of changing the transformation coefficient of the inverter transformer  $k_{\mathrm{T}}.$  The authors mention some other distinuishing features of the units, and

Experimental series of electric melting		•	S/137/62/000/005/017/150 A006/A101		150
present electric circuit diagrams for both units, parameters of the equipment, and operational characteristics of a parallel self-excited inverter. There are 12 references.					
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[Abstracter's note: Comple	ete translation]		•		•
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S/105/62/000/007/003/004 E194/E455

AUTHORS:

Donskoy, A.V., Doctor of Technical Sciences, Professor,

Ivenskiy, G.V., Candidate of Technical Sciences (Leningrad)

TITLE:

Medium-frequency ionic generators for induction

heating

PERIODICAL: Elektrichestvo, no.7, 1962, 45-50

The output frequency of ionic generators is limited by the control-grid recovery time and may range from some hundreds to some thousands of cycles/sec, which is quite adequate for many metallurgical applications. The design and construction of such The parallel inverter type of circuit is commonest and when self-excited its performance depends mainly on the parameters of the phase-regulator and little on the Q-value of the load; in induction heating this is the particular advantage of the circuit over the parallel inverter with independent excitation, though independent excitation may be used to The series/parallel inverter has a capacitor in series with the load which increases the blocking angle but unfortunately also increases the peak value of the anode Card 1/3

Medium-frequency ionic ...

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Several variants of series-parallel inverter are voltage. The grid circuit design determines the deionization described. process, which usually imposes limitations on the output frequency; design features that can increase this frequency are reviewed. For example, while the inverse voltage is on the anode, the grid resistance may be shunted by a special electronic-impulse device, which permits the output frequency to be raised without also The frequency may be raised by a increasing the grid current. suitable choice of method of connecting the secondary of the grid transformer to the valves. The blocking angle may be increased artificially by connecting saturating chokes in series with the Considerable increase of valves and RC circuits in parallel. frequency is possible with multi-stage generators and frequencydoubling circuits are described. The operation of damped-wave . impulse type are particularly suitable. Available valves and their design are described; the best existing types are TP1-6/15 (TR1-6/15) and TP1-15/15 (TR1-15/15). Their control grid recovery time is not greater than 50 microseconds and they have been used in prototype damped-wave impulse generators of Card 2/3

Medium-frequency ionic ...

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40 kW and 10 kc/s. Double-grid mercury thyratrons have been developed at the Leningradskiy elektrotekhnicheskiy institut im. Ul'yanova (Lenina) (Leningrad Electrical Engineering Institute imeni Ul'yanov (Lenin)). Hydrogen thyratrons have the best frequency characteristics but the permissible d.c. component of anode current is low and both the gas-filled and the hydrogen types have short life. Mercury ignitrons and excitrons look most promising in this respect and some recent designs are described. Although promising prototypes have been made, regular production of new valves is lagging and this hinders the development of induction heating. Westinghouse "Trinistors" are described. Semiconductor devices have little overload capacity and accordingly the associated circuitry is complicated by the need for protective devices. There are 6 figures.

SUBMITTED: February 8, 1962

Card 3/3

DONSKOY, A.V., doktor tekhn.nauk; IVENSKIY, G.V... kand.tekhn.nauk

Characteristics of a parallel inverter with self-excitation and induction heating. Vest.elektroprom. 33 no.4:39-43 Ap '62.

(MIRA 15:4)

(Electric current converters)

DONSKOV, A.V., doktor tekhin. nauk; IVEMSKIY, G.V., kand. tekhin. nauk

Transistor wattmeter for high-frequency systems. Elektrotekhnika
35 no.7:44-46 164.

(MIRA 17:11)

L 27976-66 EWT(m)/T DJ	
ACC NR: AP6017733	SOURCE CODE: UR/0066/65/000/006/0048/0049
AUTHOR: Ivenskiy, Ya. B.	26 B
ORG: Leningrad Repair and Assemb (Leningradskiy remontnomontazhnyy	bly Combine of the 'Rostormontach' Trust y kombinat tresta Rostorgmontach)
TITLE: Bellowsless gland with st	teel-to-steel friction rings \\
SOURCE: Kholodil naya tekhnika,	no. 6, 1965, 48-49
TOPIC TAGS: gas compressor, free treatment	on, refrigeration equipment, steel, metal heat
packing glands with steel-steel f bellows glands in small freon com friction ring attached to the rot stationary friction ring in the g provided by proper heat treatment	and Installation Combine has developed bellowsless friction rings, designed to replace the unreliable mpressors in IF and FAK refrigeration units. A tating compressor shaft is spring-pressed onto a gland, made of steel of different hardness, so t of the metal. Both rings are rubber-buffered of the new units allows a savings of 50% in cost. art. has 1 figure. [JFRS]
SUB CODE: 13 / SUBM DATE: non	

IVENSKIY, Yu.N., inzh.; TULLER, A.C., inzh.

Designing control systems with weak-current equipment. Mash.
Bel. no.2:54-60 '60. (MIRA 16:7)

(Electric controllers)

APPROVED FOR RELEASE. US, 20, 2002

DESCRIPTION OF THE PROPERTY OF THE PROPERT IVENSKIY, Yu. N., TULLER, A.G. Installing the electric equipment of automatic machine-tool lines. Stan.i instr. 31 no.4:29-31 Ap '60. (Electric wiring) (MIRA 13:6)

S/110/60/000/009/008/008 E194/E455

9,2/40 AUTHORS:

Ivenskiy, Yu.N., Engineer and Tuller, A.G., Engineer

TITLE:

Improving the Reliability of Relay-Contact Control

Circuits

PERIODICAL: Vestnik elektropromyshlennosti, 1960, No.9, pp.65-68

TEXT: For many types of control circuit the ordinary a.c. relay using relatively heavy currents has numerous disadvantages. This is particularly so when the number of contacts in the system runs into hundreds. The number of switching elements required to carry out executive functions in a control system is usually quite small; most of the switching elements handle the main functional relationships, requiring only signals of low power. Accordingly it is advisable to subdivide the system into two parts, one for control and the other executive. Several types of communication relay are recommended for use in circuits of this kind. When communication equipment is used, the structure of the control systems can be greatly simplified and contact wear can be reduced. The tendency to reduce the number of contacts leads to the Card 1/3

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Improving the Reliability of Relay-Contact Control Circuits

application of new elements and new methods of constructing relay control circuits. Semiconductor instruments of small size are particularly valuable. When a number of contacts of a given type but in different circuits are connected in parallel, they can easily be unified by the use of a valve. Typical circuits for this case By using additional resistances it is possible to are given. combine the functional possibilities of normally-open and normallyclosed contacts. In order to use additional resistances so as to reduce the number of contacts, certain equivalent circuits must be A number of relationships that such equivalent circuits must observe are stated. Examples are then given of the use of additional resistors and equivalent circuits to cut down The conditions of use of the apparatus the number of contacts. and contacts in the circuits have a considerable influence on the Various arc-extinguishing circuits may be used, reliability。 It is important to protect the circuit elements correctly. Protection of d.c. control circuits containing elements of very different ampere-second characteristics makes it necessary to break Card 2/3

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Improving the Reliability of Relay-Contact Control Circuits

down the control circuit into individual parts consisting of switching elements of approximately equal ampere-second characteristics. A typical control circuit arranged in this way is described. There are 6 figures.

SUBMITTED: December 10, 1959

VB

Card 3/3

s/121/60/000/011/002/013 A004/A001

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AUTHORS:

Ivenskiy, Yu. N., Tuller, A. G.

TITLE:

Check and Interlock Systems in Automatic Machine Tool Lines

PERIODICAL: Stanki i Instrument, 1960, ANO. 11, pp. 3-5

The authors present a survey of various check and interlock systems which are used for automated machine tools and transfer lines and point out that, although there is a great variance of such systems, they can be divided into three main groups: 1) Devices checking the location of individual objects and permitting their reciprocal displacement only under certain conditions. 2) Devices checking the state of objects or line apparatus (e.g. line speed, pressure of pneumatic or hydraulic systems etc.). 3) Devices for the measurement check of components being machined. The SKB-8 of the Minskiy zavod avtomaticheskikh liniy (Minsk Plant for the Manufacture of Automatic Transfer Machine Lines) uses for their checking and interlock systems to a great extent electronic units: resistors, capacitors, transistors and triodes, which makes it possible to build highly reliable miniature systems. The use of amplifiers on the base of these elements enables the requirements towards pickups as to their sensitivity and amplification

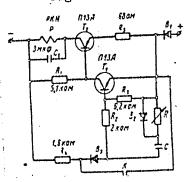
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Check and Interlock Systems in Automatic Machine Tool Lines

coefficient to be considerably lowered. The SKB-8 has developed transistor-type miniature static time relays which make it possible to obtain a time delay during the switching on or off. The command of relay operation is given in the normally open or normally closed state by the controlling contact. Figure 1 shows the circuit of a switch-off time-delay relay, where the telephone relay P is located circuit of a switch-off time-delay relay, where the telephone relay P. Stoure 2:

circuit of a switch-off time-delay relay, where and in the triode collector circuit T. This relay is normally switched on, since the triode is open. Figure 2 shows a switch-on time-delay relay composed of the triodes T<sub>1</sub> and T<sub>2</sub>. The maximum time-delay errors at temperature variations in the range of 0 to 45°C do not exceed ± 11% relative to the delay whose magnitudes are shown in tables 1 and 2. When the switch-on time-delay relay is supplied from a source with a 3-phase rectifying circuit the maximum error does not exceed ± 4%. The SKB-8 has developed a simple device to check the tool wear, which is based on a step-by-step selector. Figure 3 shows the electric circuit of the tool wear



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Check and Interlock Systems in Automatic Machine Tool Lines

check device which effects the displacement of the step-by-step selectors, signal transmission and setting of the control selector on any number of cycles. The 147 (1ShI) reference input selector is switched on by the 1P (1R) relay which in turn, is switched on if the tool presses on the terminal switch K3 (KV). At a given position of the 1ShI reference input selector, it switches on the 2450 (2SaI) slave selector acting on a signal lamp. After another revolution of the reference input selector the line is stopped. The use of tools which are by their special characteristics more subjected to break-downs has to be checked in a most efficient way. For this purpose transistor-type amplifiers have been developed. The electric contact between gage feeler and end of the checked tool (drill) is used as pickups. Owing to the high amplification coefficient a soiling of the contact spot or even the pressing stress of the gage feeler on the drill do not play any rôle. Figure 4 shows the amplifier circuit for the checking of breakdowns of two drills used in one machine tool. Relay P is switched on and permits the line

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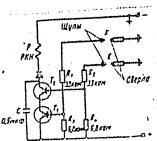
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Check and Interlock Systems in Automatic Machine Tool Lines

to operate only in that case if there is a contact between the gage feelers and the two drills. At a temperature of 40° and a voltage increase by 25% relative to the 24 v standard voltage, the maximum current passing through the gage feelers does not exceed 0.9 milliampere. If there is no contact between one gage feeler and not exceed 0.9 milliampere, while tool the current passing through the relay does not exceed 0.5 milliampere, while in the case of the two contacts existing, at a temperain the case of the two contacts existing, at a tempera-

ture of 15° and a lowering of the voltage by 15%, the current magnitude amounts to not less than 11 milli-ampere which is sufficient to operate the type FKH ampere which is sufficient to operate the type FKH (RKN) relay. For dimensional checks of machined components the models 58-779 (BV-779U) and 58-634 (BV-634U) electrocontact pickups have been widely used. Figure 5 shows the two-stage semiconductor amplifier for the electrocontact pickups and the amplifier circuit. These pickups ensure high-precision measurement and permit on their contacts a load of



Card 4/5

PERIODICAL: Stanki i Instrument,	utomatic Transfer Lines
TITLE: The Alarm System in Auprenion Periodical: Stanki i Instrument,	utomatic Transfer Lines
PERIODICAL: Stanki i Instrument,	utomatic Transfer Lines
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	1960, No. 12, pp. 1-3
transfer lines devised for the qui out that these alarm systems can b	ect 1)  per product of the left for the left
light. The use of flashing light extends the functional possibility of indicator lights, since in this	ies 2p 1p Jemann Jit Jp

THE STREET COLOR THROUGH CHIRDREST FROM THE FROM DEALERS AND THE STREET FROM THE PROPERTY OF T 87949 S/121/60/000/012/001/015 A004/A001 The Alarm System in Automatic Transfer Lines case the pilot lamps can burn in the following three stages: 1. half-indandescent burning proving the intactness of the lamps; 2. fully incandescent burning showing the normal state of the unit being checked; 3. flashing-light burning indicating a defect in the controlled unit. Figure 2 shows a circuit developed by the SKB-8 of the Minskiy zavod avtomaticheskikh liniy (Minsk Plant of Automatic Transfer Lines) for the control and signalling of the initial position taken only by one normally open contact of the terminal switches of Figure 3: the machines. Two intermediate relays are used independently of the number of machines being controlled. The control of the participation of the machine in the preceding cycle is effected either as a control of the termination of the machining process of the component or, in the time function, as a control of the beginning of the cycle. The circuit shown in Figure 3 combines the control of the initial position and participation of the 2cmanas machine in the preceding cycle. This circuit operates in such a way that the pilot lamps are burning halfincandescent if the machine is not in the initial position, while the lamps are burning brightly if the machine is Зестана Card 2/5

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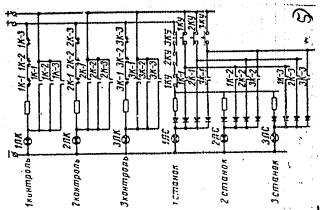
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The Alarm System in Automatic Transfer Lines

the fixed position of the movable units, while the half-incandescent burning lamps indicate those motions, delays or stops which in the intermediate position caused the line being stopped. A great number of signalling lamps on the central control panel renders observation difficult. One efficient way of reducing the number of lamps is to use the  $\Pi\Pi$ -36 (PP-36) slide switch. In this case the lamps located on the panel pertain only to one machine

Figure 5:

the panel pertain only to one machine tool, while the selection of the machine tool is carried out by the slide switch. An easy-to-watch alarm system is obtained according to the circuit shown in Figure 5. In the case of a great number of control devices only one lamp ILS, 2LS, 3LS, is fitted for each machine tool. These lamps generally burn half-incandescent. A number of buttons 1KY (1KU), 2KU, 3KU ect., depending on the number of units and operations being controlled, are



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